

Fig.1. Three points loading and geometry of artificial notch in cross section of specimen center; (a) STNSCB specimen, (b) CCNSCB specimen.



Fig.2 A finite element mesh and geometry of chevron notch: (a) 3D FEM model, (b) crack front with corners (Red circles), (c) modified crack front (Ayarollahi et al. 2016).



Fig.3 Typical linear traction-separation response.



Fig.4 XFEM model: (a) cross section on the y-z plane, (b) perspective view of the crack front geometry in the x-y plane, (c) three dimensional view.

Table 1. Geometric and mechanical parameters.

Geometric parameter	value		Mechanical parameter	value
Radius of specimen R	37.5mm		Young's modulus E	7.7GPa
Thickness of specimen t	30.0mm	t/R = 0.8	Poisson's ratio $\nu$	0.22
Support distance 2s	60.0mm	s/R = 0.8		
Initial crack length $a_0$	11.25, 18.75mm	$a_0/R = 0.3, 0.5$		
Chevron angle $\theta$	Straight, 90, 75 de	egrees		

Table 2. Number of node and element of each model.

	STNSCB	CCNSCB(90)	CCNSCB(75)
Number of node	787469	125045	125045
Number of element	114209	111080	111080



Fig.5 Comparison of load-displacement curve obtained from STNSCB test for sandstone with that by the XFEM analysis using model of STNSCB.



Fig.6 State of crack propagation at a moment of the numbers in Fig.5.



Fig.7 Cross sectional geometry of crack front during crack propagation of STNSCB test.



Fig.8 Load-crack length curve of STNSCB test.



Fig.9 Load-displacement curve and states of crack propagation of CCNSCB specimen with a chevron angle of 90 degrees. Right figures represent the state of crack propagation at a moment of 1:  $P_{\text{max}}$ = 90kN, 2: 500kN and 3: 633kN.



Fig.10 Load-displacement curve and states of crack propagation of CCNSCB specimen with a

chevron angle of 75 degrees. Right figures represent the state of crack propagation at a moment of 1:  $P_{\text{max}}$  = 90kN, 2: 310kN and 3: 574kN.



Fug. 11 Relationship between load and normalized crack length a/R of CCNSCB models in the XFEM analysis.



section of the crack front geometry

Fig.12 An example of FEM model of CCNSCB specimen with a crack length of a/R=0.38 of chevron angle of 90 degrees.



Fig.13 Distribution of normalized stress intensity factor along crack front shown in Fig.7 with increasing crack length in the STNSCB test.



Fig.14 Relation between normalized stress intensity factor and normalized crack length in STNSCB test.



Fig.15 Cross-sectional geometry of the crack front for each crack length of the CCNSCB specimen with a chevron angle of 90 degrees obtained from the XFEM analysis.



Fig. 16 Distributions of stress intensity factor in the range of 0.3 to 0.55.



Fig.17 Relationship between normalized stress intensity factor with respect to a/R in the CCNSCB

specimen with a chevron angle of 90 degrees.



Fig.18 Cross-sectional geometry of the crack front for each crack length of the CCNSCB specimen with a chevron angle of 75 degrees obtained from the XFEM analysis.



Fig. 19 Distributions of stress intensity factor in the range of 0.3 to 0.55.



Fig.20 Relationship between normalized stress intensity factor with respect to a/R in the CCNSCB specimen with a chevron angle of 75 degrees.

Material property	Values
Uniaxial compressive strength	59.3 MPa
Young's modulus	7.7 GPa
Poisson's ratio	0.22
Tensile strength	6.17 MPa
Elastic wave velocity	2.6–2.9 km/s

Table 3 Material properties of Kimachi sandstone.



Fig.21 Examples of fractured surface of STNSCB and CCNSCB specimens after test: (a) CSNSCB specimen, (b) CCNSCB specimen with a chevron angle of 90 degrees, (c) 75 degrees, (d) photo from an oblique direction.





Fig.23 Load and AE event rate – displacement curves: (a) STNSCB test (b) CCNSCB test with a chevron angle of 90 degrees during the test.



Fig.24 Load-displacements curves obtained SCB test: (a) STNSCB specimen, (b) CCNSCB specimen with a chevron angle of 90 degrees and (c) 75 degrees.

No. Radiu <i>R</i> , mi	Radius	Thickness Crack length	Crack length	$a_0/\mathbf{D}$	2 <i>S</i> / <i>R</i>	$Y_{\mathrm{I}}$	Max. load	Fracture toughness
	<i>R</i> , mm	<i>t</i> , mm	<i>a</i> <sub>0</sub> , mm	<i>u</i> 0/ <i>K</i>			P <sub>max</sub> , kN	$K_{\rm IC},  {\rm MN}/{\rm m}^{3/2}$
1	37.5	30.4	19.8	0.53	0.8	7.09	0.93	0.72
2	37.5	30.4	19.8	0.53	0.8	7.09	0.92	0.71
3	37.5	30.9	19.7	0.53	0.8	7.04	0.89	0.67
4	37.5	30.9	19.6	0.52	0.8	7.00	0.99	0.74
5	37.5	31.5	19.7	0.53	0.8	7.04	0.98	0.73

Table 4 Results of STNSCB test.

Remarks: Y<sub>I</sub> was calculated by the original formulation of ISRM (Kuruppu, Obara et al. 2014).

Table 5 Results of CCNSC	CB(90)	test.
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No. Radius $R, mm$	Radius	Thickness C	Crack length	$q_0/\mathbf{P}$	2 <i>S</i> / <i>R</i>	$Y_{\rm I}$	Max. load	Fracture toughness
	<i>R</i> , mm	<i>t</i> , mm	<i>a</i> <sub>0</sub> , mm	<i>u</i> 0/ <b>N</b>			P <sub>max</sub> , kN	$K_{\rm IC},  {\rm MN}/{\rm m}^{3/2}$
1	36.4	30.6	10.7	0.29	0.8	5.26	0.77	0.69
2	36.3	31.6	10.0	0.28	0.8	5.26	0.79	0.69
3	36.6	31.2	11.1	0.30	0.8	5.26	0.89	0.78
4	36.2	30.9	10.1	0.28	0.8	5.26	0.78	0.70
5	37.1	30.0	11.1	0.30	0.8	5.26	0.79	0.72

## Table 6 Results of CCNSCB(75) test.

No.	Radius <i>R</i> , mm	Thickness <i>t</i> , mm	Crack length <i>a</i> <sub>0</sub> , mm	$a_0/R$	2 <i>S</i> / <i>R</i>	$Y_{\rm I}$	Max. load P <sub>max</sub> , kN	Fracture toughness $K_{\rm IC}$ , MN/m <sup>3/2</sup>
1	35.7	30.1	10.7	0.30	0.8	6.58	0.58	0.67
2	36.0	30.4	10.8	0.30	0.8	6.58	0.72	0.82
3	36.8	30.4	11.4	0.31	0.8	6.58	0.74	0.83
4	36.3	30.9	11.3	0.31	0.8	6.58	0.70	0.78



Fig 25 Fracture toughness of Kimachi sandstone estimated by the specimen with different artificial notch shape.